

ON A CYLINDRICAL BODY IN A NONLINEAR MEDIUM PLANE SHOCK WAVE EFFECT

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Abstract

In this article, the effect of one-dimensional waves on a non-deformable moving cylinder located in the ground is studied. The environment model is taken as a grunt [1]. The article defines the kinematic parameters of the cylindrical structure and the stresses generated around the cylinder. According to this model, the relationships between stress and deformation obtained based on experience are assumed to be homogeneous during loading and unloading, that is, the environment is nonlinear. The problem is reduced to a Cauchy problem based on suitable initial conditions. The results of the issue will be presented in the next article.

Introduction

The effect of seismic waves on underground structures is one of the most urgent and important issues. If these structures are cylindrical, then underground metro, oil, water and gas pipelines are one such example. Cylindrical underground devices are the most common structures in practice.

Ensuring their strength, integrity and stability is of great importance in construction. Many scientists from Uzbekistan have dealt with such issues. [2, 3, 4, 5, 6, 7].

Setting the issue. Let the shock wave front arrive at the cylinder along the OX axis at the time of initiation, i.e. at $t=0$. In the considered problem, we accept the condition of adhesion, that is, the displacements of any point attached to the cylinder and the points touching it are equal to each other.

For the medium in which the cylinder is located, we obtain the following relations obtained based on experiments such as [1]:

$$\lambda(\varepsilon, \varepsilon_i) = \alpha_1 - \alpha_2 \varepsilon - \frac{2}{9}(\beta_1 + \beta_2 \varepsilon_i), \quad G = \frac{1}{3}(\beta_1 + \beta_2 \varepsilon_i) \quad (1)$$

This is for fine-grained sands: $\alpha_1 = 18 \cdot 10^2 \text{ kg/sm}^2$, $\alpha_2 = 82 \cdot 10^3 \text{ kg/sm}^2$,

$$\beta_1 = 42 \cdot 10^2 \text{ kg/sm}^2, \quad \beta_2 = 18 \cdot 10^4 \text{ kg/sm}^2$$

The voltage behind the shock wave front $X_x = -P_0$ ($(P_0 > 0 - \text{const})$ and its speed $D = \text{const}$) let it be

In this case, the following relations are valid for the shock wave.

$$\begin{cases} \rho_1(D - V_x) = \rho_0 D \\ \rho_0 D V_x = -X_x \\ \rho_0 = \rho_1(1 + u_x) \end{cases} \quad (2)$$

If $X_x = -100 \frac{\text{kg}}{\text{cm}^2}$, $\rho_0 = 200 \frac{\text{kg} \cdot \text{cm}^2}{\text{m}^4}$ if, then $D = 545 \frac{\text{m}}{\text{s}}$, $V_x = 9,17 \frac{\text{m}}{\text{s}}$, $\rho_0 = 203,42 \frac{\text{kg} \cdot \text{cm}^2}{\text{m}^4}$ will be equal to it is appropriate to work on this problem, i.e., the effect of the wave on the cylinder, in the cylindrical coordinate system. The displacements in the radial and transverse directions behind the shock wave front will have the following form:

$$\begin{aligned} u(r, \theta, t) &= -10^{-2} \cdot 1,682[(r_0 + r) \cos \theta - Dt + r_0] \cos \theta; \\ v(r, \theta, t) &= -10^{-2} \cdot 1,682[(r_0 + r) \cos \theta - Dt + r_0] \sin \theta; \end{aligned} \quad (3)$$

Particle velocities are determined by the following formulas:

$$\dot{u} = V_x \cos \theta, \quad \dot{v} = V_x \sin \theta$$

To create the equations of motion of the environment, we cover the plane along the radial and perpendicular lines from the origin of the coordinate with rectangles with imaginary curves. The radii of concentric circles are determined as follows:

$$r_0 + r_k \text{ in this } r_k = \frac{2k-1}{2} \cdot \Delta r, \quad (k=1, 2, \dots, \Delta r = \frac{b-r_0}{n_1}, \quad b \text{ fictitious outer radius}).$$

We define polar angles as follows.

$$\theta_s = \frac{2s-1}{2} \cdot \Delta \theta \quad (\Delta \theta \text{-are angles corresponding to curved elements}). \text{ It is optional}$$

after it $(r_0 + r_k, \theta_s)$ the equations of motion of the elements are drawn up. The stresses on the four sides of the centers of the resulting elements are written based on finite differences. The resulting tensions $\sigma_{rr}[r_0 + k \cdot \Delta r, \theta_s]$, $\sigma_{r\theta}[r_0 + r_k, s \cdot \Delta \theta]$, $\sigma_{\theta\theta}[r_0 + r_k, s \cdot \Delta \theta]$, $\sigma_{r\theta}[r_0 + k \cdot \Delta r, \theta_s]$ expressions are not given here because they are complicated. Since the problem is symmetrical, it is appropriate to work on it and the field.

The mass of isolated elements $m_{k,s}$ - we get the following system of differential equations in the radial and tangential directions:

$$\begin{aligned}
 m_{k,s} \ddot{u}_{k,s} = & -\sigma_{rr} [r_0 + \Delta r(k-1), \theta_s] [r_0 + \Delta r(k-1)]' \Delta \theta + \sigma_{rr} [r_0 + \Delta r, k / \theta_s] \cdot \\
 & \cdot [r_0 + \Delta r k] \Delta \theta - \sigma_{r\theta} [r_0 + r_k, (s-1) \Delta \theta] \Delta r \cos \frac{\Delta \theta}{2} + \sigma_{r\theta} [r_0 + r_k, s \Delta \theta] \Delta r \cos \frac{\Delta \theta}{2} - (4) \\
 & - \sigma_{\theta\theta} [r_0 + r_k, (s-1) \Delta \theta] \cdot \sin \frac{\Delta \theta}{2} - \sigma_{\theta\theta} [r_0 + r_k, s \Delta \theta] \Delta r \sin \frac{\Delta \theta}{2} \\
 m_{k,s} \ddot{v}_{k,s} = & -\sigma_{\theta\theta} [r_0 + \Delta r(s-1), \Delta \theta] \Delta r \cos \frac{\Delta \theta}{2} + \sigma_{\theta\theta} [r_0 + r_k, s \Delta \theta_s] \cdot \\
 & \Delta r \cos \frac{\Delta \theta}{2} - \sigma_{r\theta} [r_0 + (k-1) \Delta r, \theta_s] [r_0 + (k-1) \Delta r] \Delta \theta + \sigma_{r\theta} [r_0 + k \Delta r, \theta_s] \cdot \\
 & \Delta r \cos \frac{\Delta \theta}{2} - \sigma_{r\theta} [r_0 + (k-1) \Delta r, \theta_s] [r_0 + (k-1) \Delta r] \Delta \theta + \sigma_{r\theta} [r_0 + k \Delta r, \theta_s] \cdot \\
 & \cdot (r_0 + k \Delta r) \Delta \theta + \sigma_{\theta\theta} [r_0 r_k, (s-1) \Delta \theta] \Delta r \sin \frac{\Delta \theta}{2} + \sigma_{r\theta} [r_0 + r_k, s \Delta \theta] \Delta r \sin \frac{\Delta \theta}{2}
 \end{aligned}$$

For a cylinder of mass M , we construct its equation of motion:

$$M \ddot{u}_0 = \frac{2\pi r_0}{n_1} \sum \{ \sigma_{rr} [r_0, \theta_i] \cos \theta_i - \sigma_{r\theta} [r_0, \theta_i] \sin \theta_i \} \quad (5)$$

In this $u_0(t)$ is the displacement of the center of mass of the cylinder along the axis; - the number of divisions of a circle with a radius.

Within the boundaries of the cylinder, i.e $r = r_0$ the following conditions are met:

$$u_{k,s} = u_0 \cos \theta_s, \quad v_{k,s} = -u_0 \sin \theta_s$$

$r_0 \leq r \leq b$ in the field, the movements of particles in the cylinder and system are expressed by equations (4) and (5). $r = b$ va $0 \leq \theta \leq \arccos((Dt - r_0)/b)$: $u_{k,s} = v_{k,s} = 0$ will be. If $\arccos((Dt - r_0)/b) \leq \theta \leq \pi$ and in the field σ_{rr} , $\sigma_{r\theta}$, $\sigma_{\theta\theta}$ voltages are calculated by incident wave formulas. The system of equations created in this way is closed. The initial conditions are defined based on conditions (3) behind the front, and they are zero in front of the front.

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